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# **Exploiting Melting Point Depression for Hot Melt Extrusion Processing of Amorphous Solid Dispersions**

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# **Introduction**

In hot melt extrusion (HME) processing of amorphous solid dispersions (ASD), a homogenous molecular dispersion must be generated, avoiding both thermal degradation of drug and polymer and residual crystalline content. Applying temperature-composition phase diagrams, based on melting point depression of a miscible-drug polymer system, and taking into account kinetic criteria, rationally selected process conditions can be identified to prepare ASDs free of residual crystalline content.

# **Melting Point Depression**

### **Conclusion**

The temperature-composition phase diagram provides an rational framework for designing HME processes to manufacture ASD to prevent residual crystalline content, delineating the minimum processing temperature based on thermodynamic considerations.

This approach can be further refined by developing a process operating design space diagram which incorporates both thermodynamic and kinetic considerations, wherein processes using lower temperatures and shorter residence times are more susceptible to residual crystallinity. Accurate determination of the processing regime zone boundaries lessens the risk of residual crystallinity, and depends on the analytical approach employed.

#### **For More Information**

Moseson, DE, and LS Taylor. "The application of temperature-composition phase diagrams for hot melt extrusion processing of amorphous solid dispersions to prevent residual crystallinity." Submitted (2018).



# **Hot Melt Extrusion Results**

#### **Formulation**

50% Indomethacin, 50% PVPVA

#### **Extrusion**

Xplore PME, 5 mL corotating conveying screw at 20 rpm, 10 g batch size, independently controlled operating melt temperature and residence time

The formulation critical temperature  $(T_c)$ represents the minimum processing **PVPVA THE** temperature for a given composition, where drug crystals can dissolve/melt and mix with the molten polymer.

#### **Characterization**

Crystalline solubility ~5 ug/mL (in pH 4.5 acetate buffer), melting point  $T_m$  161°C, glass transition  $T_{g}$  44°C

X-ray powder diffraction (XRPD), differential scanning calorimetry (DSC), polarized light microscopy (PLM)



Figure 1. The temperature-composition phase diagram for a drug-polymer system can be used to guide processing temperature selection. By incorporating *kinetic criteria, a process operating design space diagram can be constructed.* 



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*Figure 2. (a) Melting point depression is illustrated through DSC heat flow traces of various drug-polymer mixtures. (b) Melting point offset temperature is nonlinear with respect to heating rate. (c) The interaction parameter*  $χ$  *can be extracted by linear regression analysis.*

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## **Acknowledgements**





Even at short residence times, a fully amorphous sample is generated. **Dissolution Regime (T<sub>m</sub>>T<sub>c</sub>)** 

$$
\left(\frac{1}{T_c} - \frac{1}{T_m}\right) = -\frac{R}{\Delta H} \left[ \ln \phi + \left(1 - \frac{1}{m}\right) \left(1 - \phi\right) + \chi \left(1 - \phi\right)^2 \right]
$$

At short residence times (2 minutes), a processing temperature of 10°C above the  $T_c$  was required to generate a fully amorphous sample. At the  $T<sub>c</sub>$ , residence time exceeding 20 minutes was required to generate a fully amorphous sample.

### **Suspension Regime (<Tc)**

Below the  $T_c$ , a fully amorphous sample could not be prepared.

dispersion Suspended drug particles dissolving Premixed drug Suspendec }uspendec at high rates and polymer drug particles drug particles OOL *Concurrent* diffusion & mixing **Insufficient** nixing and/or residence time **Dissolution Regime**  Amorphous solid dispersion with residual crystallinity

Negative Flory-Huggins interaction parameter  $\chi$  indicates favorable enthalpy of mixing & results in melting point depression

Melting point depression

For some compositions, the polymer minimum temperature  $(T_{min})$  represents a lower bound of processing temperature, due to high viscosity.

#### **Indomethacin (BCS Class 2)**

## **Polyvinylpyrrolidone/vinyl acetate copolymer (PVPVA)**

Glass transition  $T_q$  104°C



## **Materials**

# **Extrusion & Characterization Methods**

## **Experimental Phase Diagram**









The indomethacin/PVPVA system is highly miscible, as indicated by the negative interaction parameter  $\chi$ =-1.97. Approximately 30°C of melting point depression is observed at the 50% drug loading composition.

*Figure 3. Indomethacin-PVPVA temperature-composition phase diagram, identifying the solubility line and glass transition temperature across the composition range.*

*Figure 6. HME process operating design space of 1:1 indomethacin:PVPVA . Based on the sensitivity of the characterization technique, the sample can be classified as*  amorphous or crystalline. These classifications create zones where samples can be *considered amorphous.*

# **Experimental Process Operating Design Space**

*Figure 4. Quantification of crystalline content of 1:1 indomethacin:PVPVA ASDs by XRPD as a function of product melt temperature.*

### **HME Processing Regimes**





*Figure 6. Formation mechanism of ASDs by HME processed at temperatures between Tm and Tc. Residual crystallinity may result if insufficient mixing and/or residence time is provided.*



#### **Melting Regime (>Tm)**

A homogenous molecular dispersion forms if the system achieves thermodynamic solubility equilibrium, given appropriate kinetic conditions.

The risk for residual crystallinity is controlled by selection of key process variables (e.g. temperature, residence time, equipment configuration, drug particle size distribution).

The expected trends between temperature and residence time are observed, with longer residence times being required to produce amorphous samples at lower temperatures.

The crystalline-to amorphous zone transition boundary depends significantly on the measurement technique employed.